

본 사이트에서 수업 자료로 이용되는 저작물은 **저작권법 제25조 수업목적저작물 이용 보상금제도**에 의거, **한국복제전송저작권협회와 약정을 체결하고** 적법하게 이용하고 있습니다. 약정범위를 초과하는 사용은 저작권법에 저촉될 수 있으므로 **수업자료의 대중 공개·공유 및 수업 목적 외의 사용을 금지합니다.**

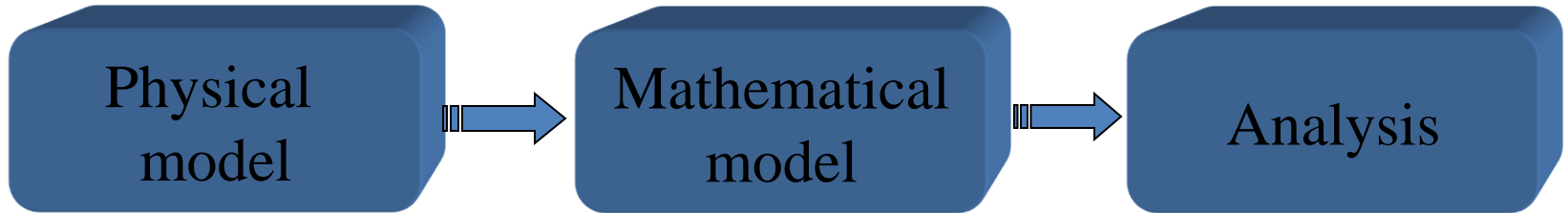
2014. 03. 24.

동아대학교·한국복제전송저작권협회

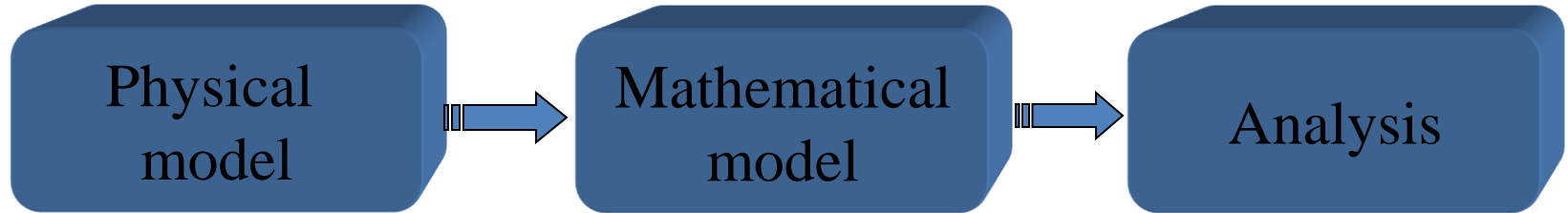
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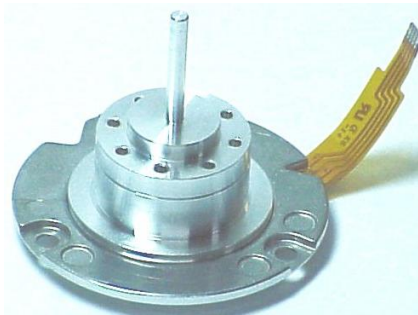
1. 모드해석이란



※ Magnetic field analysis

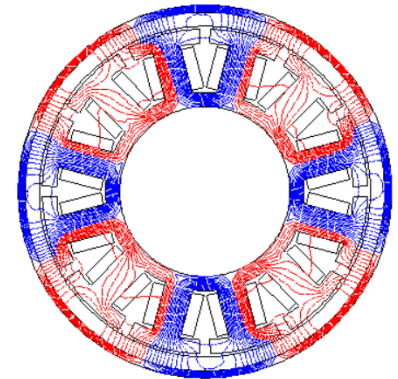


- simplification
- idealization

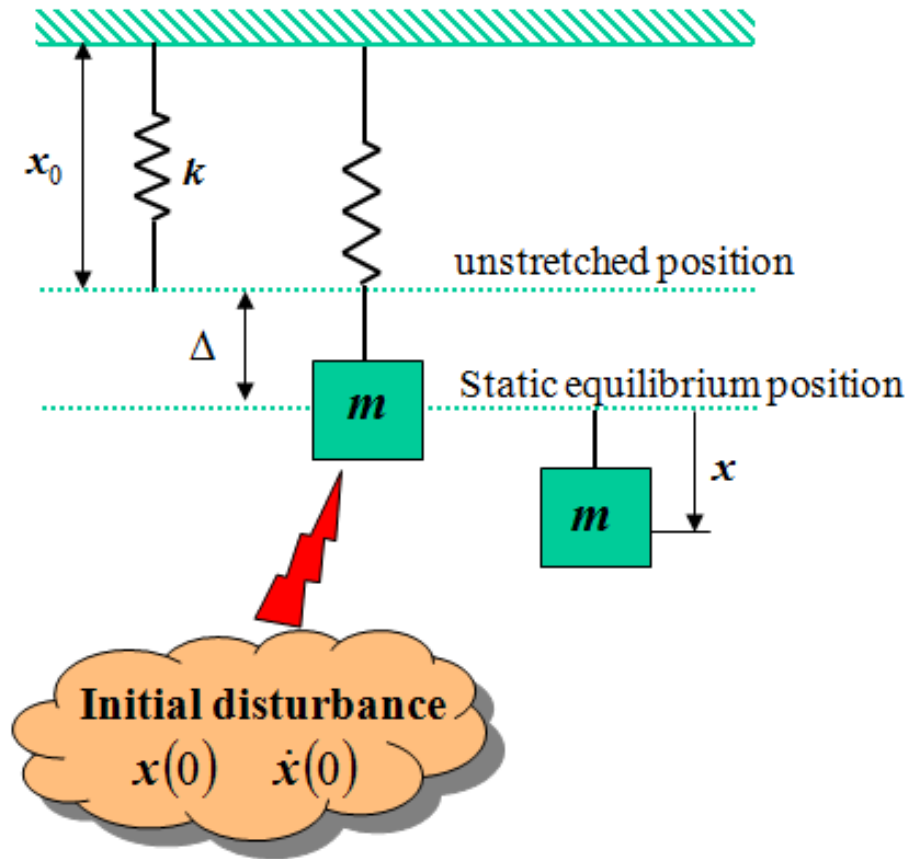


- governing equation
Maxwell equation

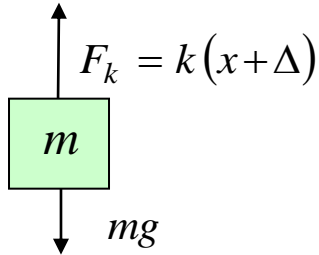
- analytical method
- numerical method



2. 1자유도 시스템의 비감쇠계 자유진동



< Free Body Diagram >



< Newton's 2nd law >

$$\sum \vec{F} = m\vec{a}$$

$$-k(x + \Delta) + mg = ma$$

$$m\ddot{x} + kx = 0$$

↖ equation of motion

equation of motion

$$m\ddot{x} + kx = 0$$

initial conditions

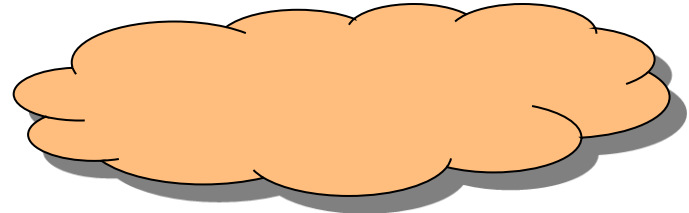
$$x(0) = x_0, \quad \dot{x}(0) = v_0$$

solution

$$x(t) = A \sin(\omega_n t + \phi)$$

$$= \frac{\sqrt{\omega_n^2 x_0^2 + v_0^2}}{\omega_n} \sin\left(\omega_n t + \tan^{-1} \frac{\omega_n x_0}{v_0}\right)$$

$$\omega_n = \sqrt{\frac{k}{m}} \quad [\text{rad/s}]$$



Displacement

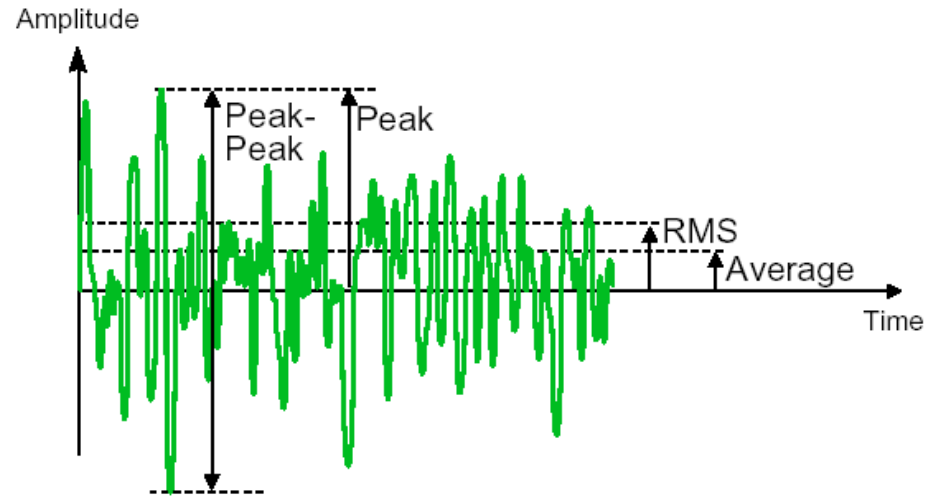
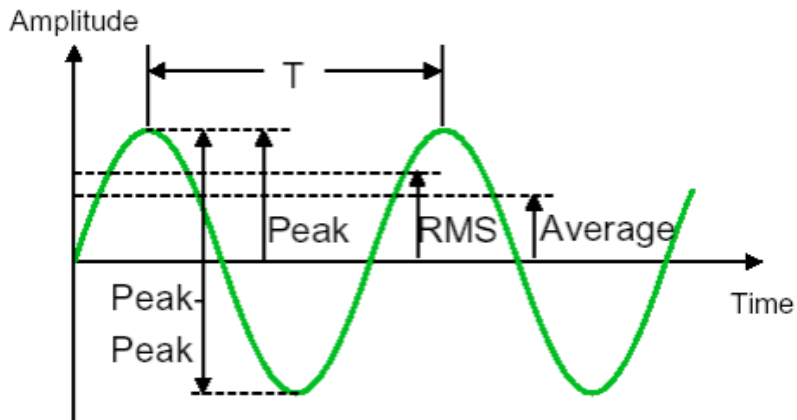
$$x(t) = A \sin(\omega_n t + \phi)$$

Velocity

$$\begin{aligned} v(t) &= \frac{d x(t)}{d t} = \omega_n A \cos(\omega_n t + \phi) \\ &= \omega_n A \sin(\omega_n t + 90^\circ + \phi) \end{aligned}$$

Acceleration

$$\begin{aligned} a(t) &= \frac{d v(t)}{d t} = -\omega_n^2 A \sin(\omega_n t + \phi) \\ &= \omega_n^2 A \sin(\omega_n t + 180^\circ + \phi) \end{aligned}$$



Period : T

$$T = \frac{2\pi}{\omega}$$

Frequency: f

$$f = \frac{1}{T} = \frac{\omega}{2\pi}$$

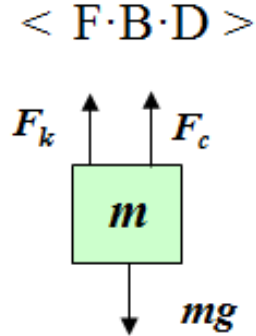
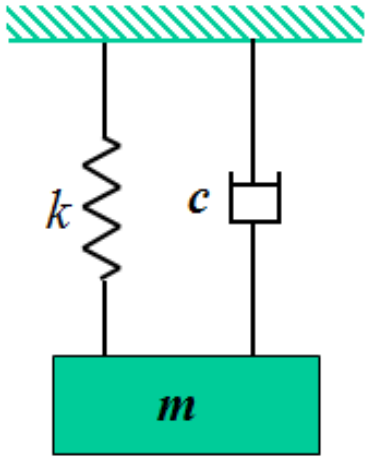
Average value

$$\bar{x} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T x(t) dt$$

Root mean square value (RMS value)

$$RMS(x) = \sqrt{\lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T x^2(t) dt}$$

3. 1자유도 시스템의 감쇠계 자유진동



$$m\ddot{x} + c\dot{x} + kx = 0 \quad (1)$$

$$x(0) = x_0, \quad \dot{x}(0) = v_0$$

$$x = ae^{\lambda t} \quad (2)$$

(2) \rightarrow (1)

$$(m\lambda^2 + c\lambda + k) ae^{\lambda t} = 0$$

$$m\lambda^2 + c\lambda + k = 0$$

$$\therefore \lambda_{1,2} = \frac{-c \pm \sqrt{c^2 - 4mk}}{2m}$$

$$\sum \vec{F} = m\vec{a}$$

$$-k(x+\Delta) - c \frac{d}{dt}(x+\Delta) + mg = m\ddot{x}$$

① critical damping

$$c_{cr} - 4mk = 0$$
$$\therefore c_{cr} = 2\sqrt{mk} \quad (4)$$

② damping ratio

$$\zeta = \frac{c}{c_{cr}} = \frac{c}{2\sqrt{mk}} \quad (5)$$

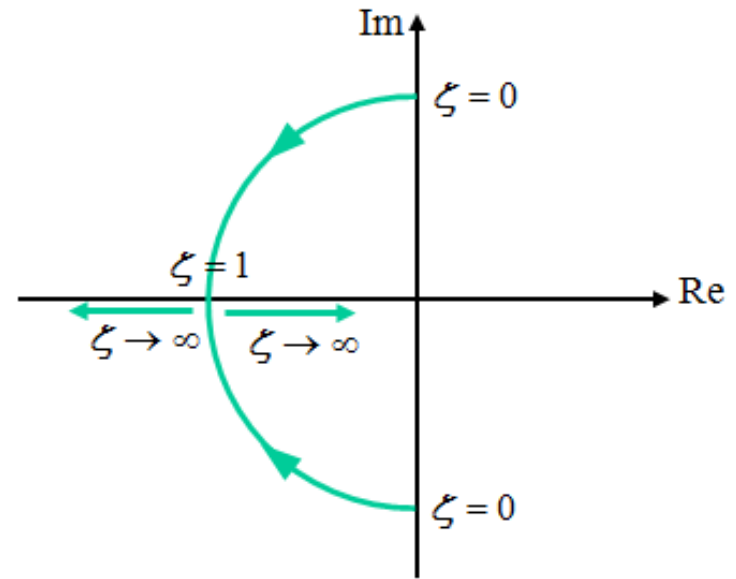
(5) \rightarrow (3)

$$\therefore \lambda_{1,2} = -\zeta \omega_n t \pm \omega_n \sqrt{\zeta^2 - 1}$$

$$0 < \zeta < 1$$

$$\zeta = 1$$

$$\zeta > 1$$



Locus of $\lambda_{1,2}$ with the variation of damping ratio

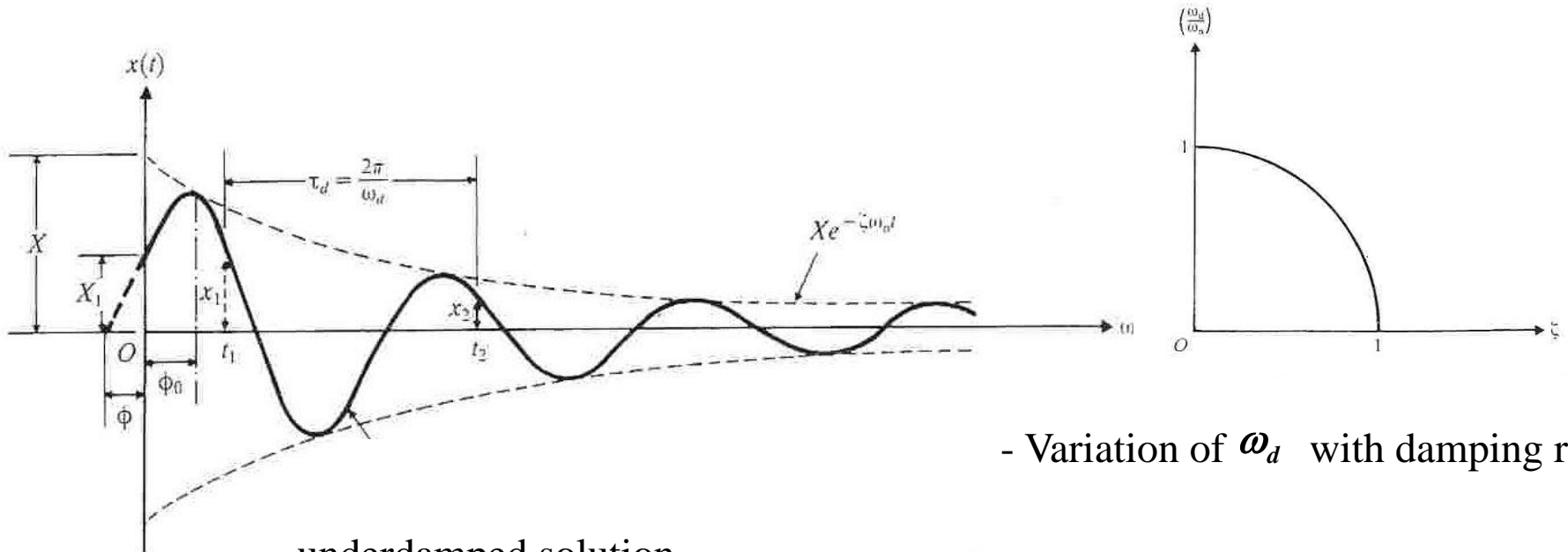
(A) underdamped system

$$\lambda_{1,2} = -\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$$

$$x(t) = e^{-\zeta \omega_n t} \left(a_1 e^{j \omega_n \sqrt{1 - \zeta^2} t} + a_2 e^{-j \omega_n \sqrt{1 - \zeta^2} t} \right)$$

$$= X e^{-\zeta \omega_n t} \sin(\omega_d t + \phi)$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2} \quad [rad / s]$$



- underdamped solution -

- Variation of ω_d with damping ratio -

(B) critically damped system

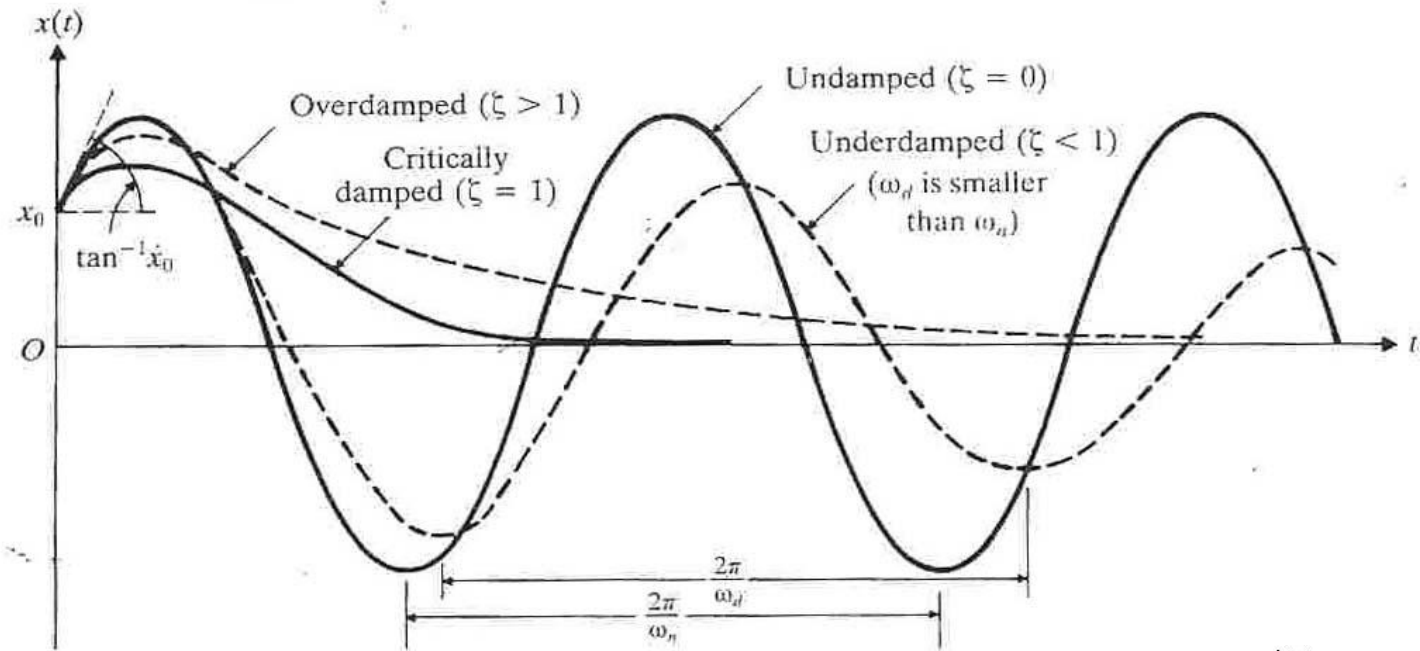
$$\lambda_{1,2} = -\omega_n$$

$$x(t) = (a_1 + a_2 t) e^{-\omega_n t}$$

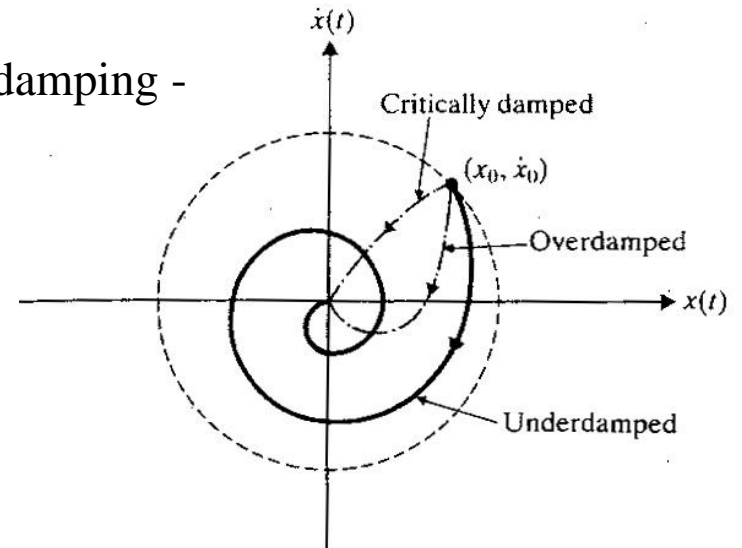
(C) overdamped system

$$\lambda_{1,2} = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

$$x(t) = e^{-\zeta \omega_n t} \left(a_1 e^{\omega_n \sqrt{\zeta^2 - 1} t} + a_2 e^{-\omega_n \sqrt{\zeta^2 - 1} t} \right)$$



- Comparison of motions with different types of damping -

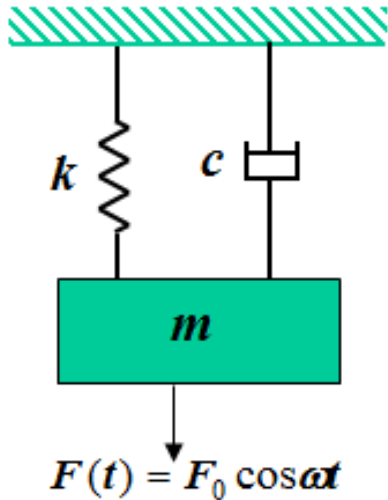


※ Energy dissipated in viscous damping

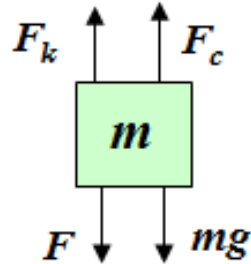
$$\begin{aligned}\frac{dW}{dt} &= \text{force} \times \text{velocity} = F \cdot v \\ &= (-cv) \cdot v \\ &= -c \left(\frac{dx}{dt} \right)^2\end{aligned}$$

$$\begin{aligned}\Delta W &= \int_0^{(2\pi/\omega_d)} c \left(\frac{dx}{dt} \right)^2 dt \\ &= \int_0^{(2\pi/\omega_d)} c \left(\frac{d(X \sin \omega_d t)}{dt} \right)^2 dt \\ &= \pi c \omega_d X^2\end{aligned}$$

4. 1자유도 시스템의 감쇠계 강제진동



< F·B·D >



$$m\ddot{x} + c\dot{x} + kx = F(t)$$

(6)

$$x(0) = x_0, \quad \dot{x}(0) = v_0$$

$$x(t) = x_h(t) + x_p(t)$$

ω :

$$\sum \vec{F} = m\vec{a}$$

$$-k(x+\Delta) - c \frac{d}{dt}(x+\Delta) + mg + F(t) = m\ddot{x}$$

(A) Undamped case

(1) $\omega_n \neq \omega$

$$\begin{aligned}x(t) &= A \sin \omega_n t + B \cos \omega_n t + \frac{F_0/m}{\omega_n^2 - \omega^2} \cos \omega t \\ &= \frac{v_0}{\omega_n} \sin \omega_n t + \left(x_0 - \frac{f_0}{\omega_n^2 - \omega^2} \right) \cos \omega_n t + \frac{f_0}{\omega_n^2 - \omega^2} \cos \omega t\end{aligned}$$

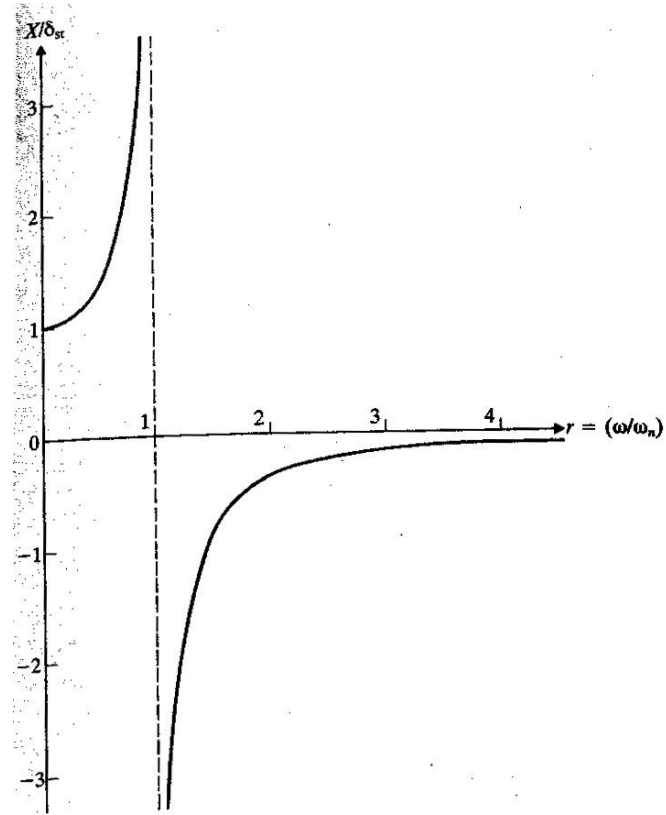
$$X = \frac{F_0/m}{\omega_n^2 - \omega^2}$$

$$\delta_{st} = \frac{F_0}{k}$$

$$\kappa = \frac{X}{\delta_{st}} = \frac{1}{1 - \left(\frac{\omega}{\omega_n} \right)^2}$$

$$(2) \quad \omega_n = \omega$$

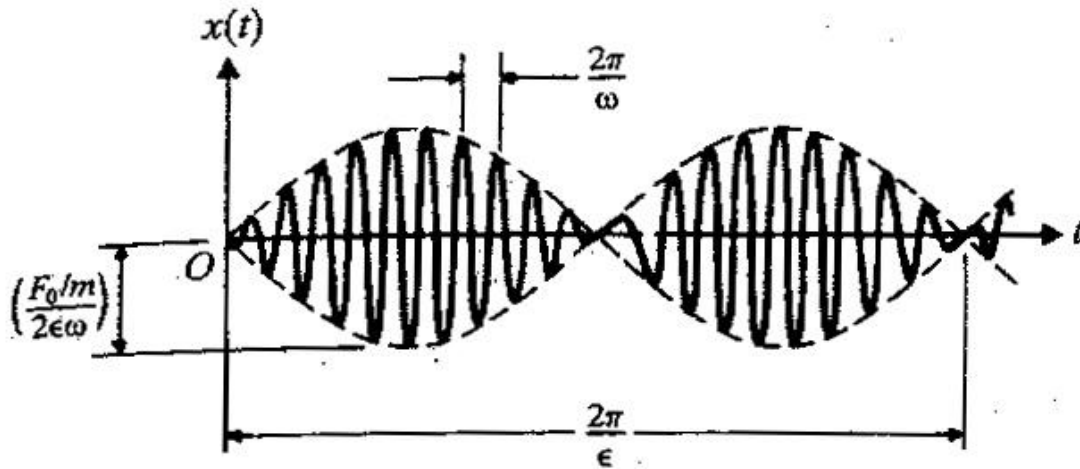
$$x(t) = A_1 \sin \omega t + B_1 \cos \omega t + \frac{f_0}{2\omega} t \sin \omega t$$
$$= \frac{v_0}{\omega} \sin \omega t + x_0 \cos \omega t + \frac{f_0}{2\omega} t \sin \omega t$$



- Variation of magnification factor with frequency ration -

(3) $\omega_n \approx \omega$ (assume $x_0 = v_0 = 0$)

$$\begin{aligned} x(t) &= \frac{f_0}{\omega_n^2 - \omega^2} (\cos \omega t - \cos \omega_n t) \\ &= \frac{2f_0}{\omega_n^2 - \omega^2} \sin\left(\frac{\omega_n - \omega}{2} t\right) \sin\left(\frac{\omega_n + \omega}{2} t\right) \end{aligned}$$



- Beating phenomenon -

Period of beating : τ_b

$$\tau_b = \frac{2\pi}{\omega_n - \omega}$$

Frequency of beating : ω_b

$$\omega_b = \omega_n - \omega$$

(B) Damped case

$$x_p(t) = X \cos(\omega t - \theta)$$

$$= \frac{f_0}{\sqrt{(\omega_n^2 - \omega^2)^2 + (2\zeta\omega_n\omega)^2}} \cos\left(\omega t - \tan^{-1} \frac{2\zeta\omega_n\omega}{\omega_n^2 - \omega^2}\right)$$

Where,

$$f_0 = \frac{F_0}{m}$$

In the steady state

Dynamic magnification factor

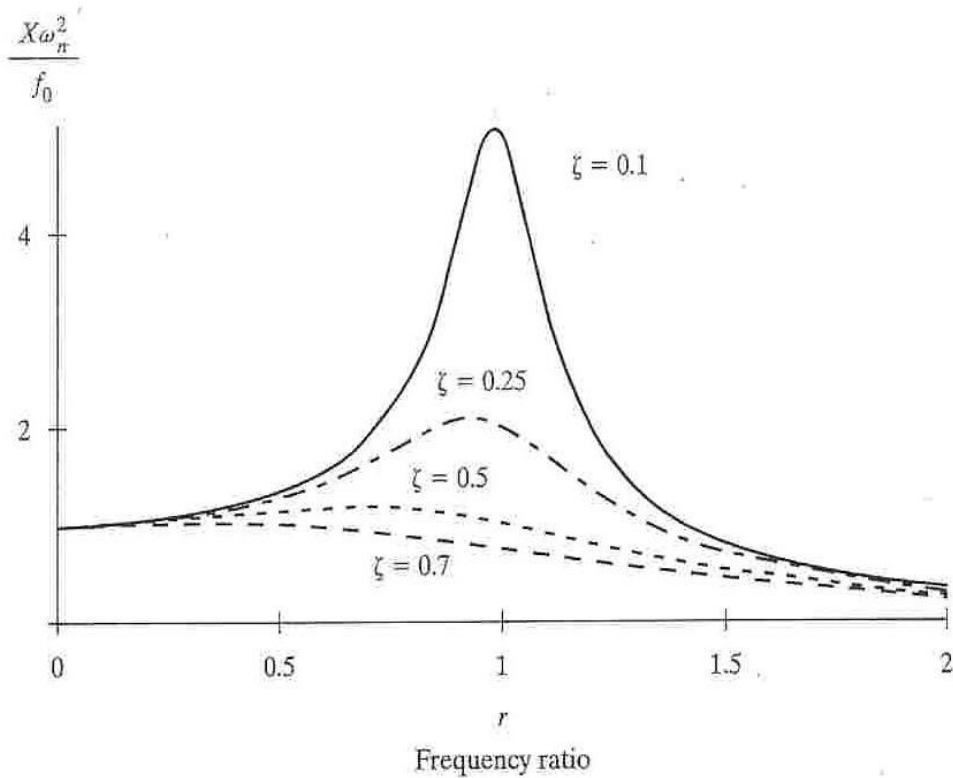
$$\kappa = \frac{X}{F_0/k} = \frac{Xk}{F_0} = \frac{1}{\sqrt{(1-r^2)^2 + (2\zeta r)^2}}$$

F_0/k : static displacement

$$r = \frac{\omega}{\omega_n}$$

Phase

$$\theta = \tan^{-1} \frac{2\zeta r}{1-r^2}$$



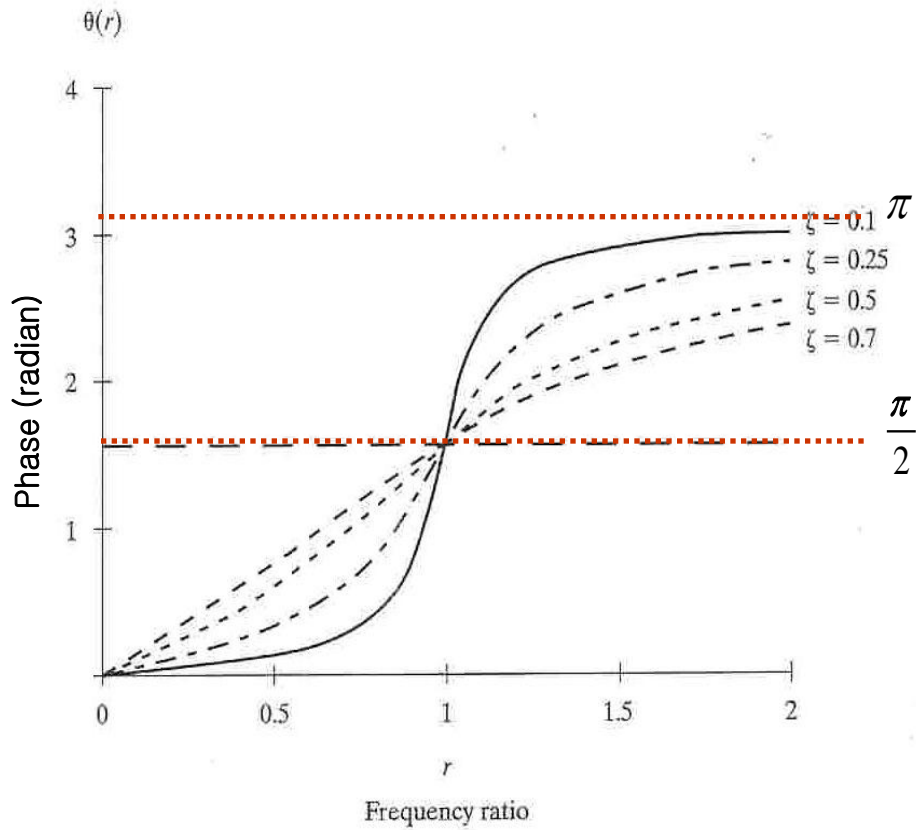
Peak magnitude of amplification factor

1) Case I $\left(0 \leq \zeta \leq \frac{1}{\sqrt{2}}\right)$

$$\kappa = \frac{1}{2\zeta\sqrt{1-\zeta^2}} \quad \text{at } r_{peak} = \sqrt{1-2\zeta^2}$$

2) Case II $\left(\zeta > \frac{1}{\sqrt{2}}\right)$

$$\kappa = 1 \quad \text{at } r_{peak} = 0$$



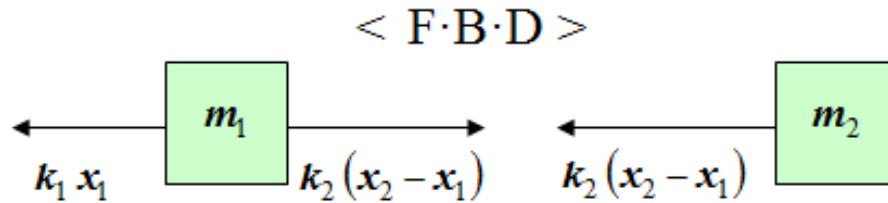
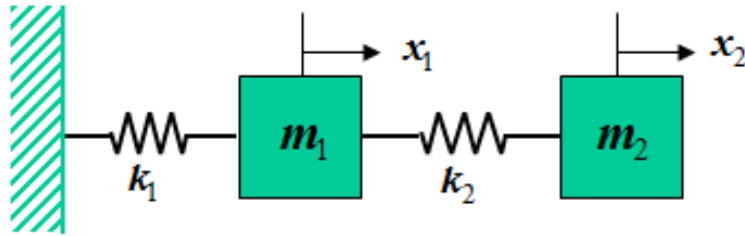
1) Case I ($\zeta = 0$)

($0 < r < 1$)
($r > 1$)

2) Case II ($\zeta > 0$)

($0 < r < 1$)
($r = 1$)
($r > 1$)

5. 다자유도 시스템의 비감쇠계 자유진동



$$\sum \vec{F} = m\vec{a}$$

$$m_1 \ddot{x}_1 + (k_1 + k_2)x_1 - k_2x_2 = 0$$

$$m_2 \ddot{x}_2 - k_2x_1 + k_2x_2 = 0$$

$$x_1(0) = x_{10} \quad x_2(0) = x_{20}$$

$$\dot{x}_1(0) = \dot{x}_{10} \quad \dot{x}_2(0) = \dot{x}_{20}$$

$$[M]\{\ddot{x}\} + [K]\{x\} = \{0\}$$

$$\{x_0\} = \begin{Bmatrix} x_1(0) \\ x_2(0) \end{Bmatrix} \quad \{\dot{x}_0\} = \begin{Bmatrix} \dot{x}_1(0) \\ \dot{x}_2(0) \end{Bmatrix} \quad (8)$$

Where,

$$[M] = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix}$$

$$[K] = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix}$$

$$\{x\} = \begin{Bmatrix} x_1(t) \\ x_2(t) \end{Bmatrix}$$

$$\{x(t)\} = \{u\}e^{j\omega t} \quad (9)$$

(9) \rightarrow (8)

$$\left(-\omega^2 [M] + [K]\right) \{u\}e^{j\omega t} = \{0\}$$

For nontrivial solution

$$\det(-\omega^2 [M] + [K]) = 0$$

$$\det \begin{bmatrix} -\omega^2 m_1 + k_1 + k_2 & -k_2 \\ -k_2 & -\omega^2 m_2 + k_2 \end{bmatrix} = 0$$

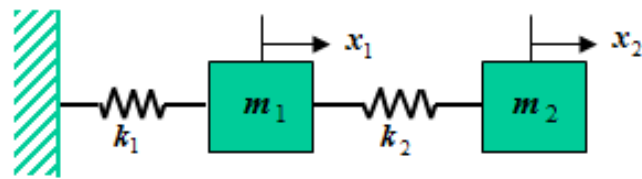
$$m_1 m_2 \omega^4 - (m_1 k_2 + m_2 k_1 + m_2 k_2) \omega^2 + k_1 k_2 = 0$$

$$\textcircled{1} \quad \omega_1^2 \quad \omega_2^2$$

$$\textcircled{2} \quad \begin{aligned} (-\omega_1^2 [M] + [K])\{u_1\} &= \{0\} \\ (-\omega_2^2 [M] + [K])\{u_2\} &= \{0\} \end{aligned}$$

By superposition principle, the general solution of the system

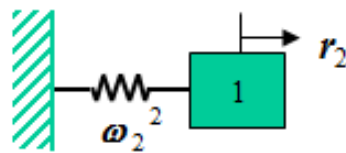
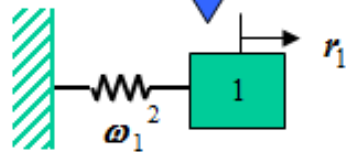
$$\begin{aligned} \{x(t)\} &= (ae^{j\omega_1 t} + be^{-j\omega_1 t})\{u_1\} + (ce^{j\omega_2 t} + de^{-j\omega_2 t})\{u_2\} \\ &= A_1 \sin(\omega_1 t + \phi_1)\{u_1\} + A_2 \sin(\omega_2 t + \phi_2)\{u_2\} \end{aligned}$$



Physical coordinate
(coupled)

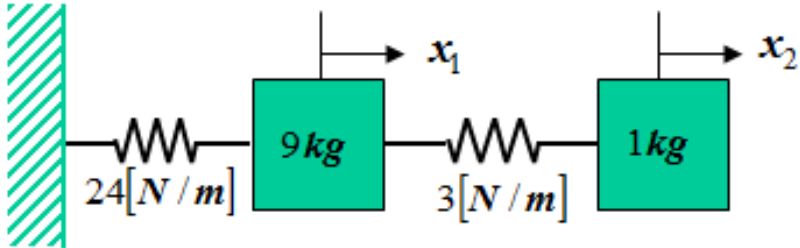


Modal Analysis



Modal coordinate
(uncoupled)

ex1)



$$x_{10} = 1[mm], \quad x_{20} = 0[mm]$$
$$\dot{x}_{10} = \dot{x}_{20} = 0$$

sol)

$$\begin{bmatrix} 9 & 0 \\ 0 & 1 \end{bmatrix} \{\ddot{x}\} + \begin{bmatrix} 27 & -3 \\ -3 & 3 \end{bmatrix} \{x\} = \{0\} \quad (9)$$

$$\{x(t)\} = \{u\} e^{j\omega t} \quad (10)$$

(10) \rightarrow (9)

$$(-\omega^2 [M] + [K]) \{u\} e^{j\omega t} = \{0\}$$

$$\det(-\omega^2 [M] + [K]) \\ = \det\left(-\omega^2 \begin{bmatrix} 9 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} 27 & -3 \\ -3 & 3 \end{bmatrix}\right) = 0$$

$$\therefore \omega_1 = \pm\sqrt{2} \text{ [rad/s]} \quad \omega_2 = \pm 2 \text{ [rad/s]}$$

$$\textcircled{1} \omega_1 = \pm\sqrt{2}$$

$$(-2[M] + [K]) \{u\} = \{0\}$$

$$\begin{bmatrix} -18+27 & -3 \\ -3 & -2+3 \end{bmatrix} \begin{Bmatrix} u_{11} \\ u_{21} \end{Bmatrix} = \{0\}$$

$$\therefore \{u_1\} = k_1 \begin{Bmatrix} 1 \\ 3 \end{Bmatrix}$$

$$\textcircled{2} \quad \omega_2 = \pm 2$$

$$(-4[M] + [K]) \{u\} = \{0\}$$

$$\therefore \{u_2\} = k_2 \begin{Bmatrix} -1 \\ 3 \end{Bmatrix}$$

$$\therefore \{x(t)\} = A_1 \sin(\omega_1 t + \phi_1) \{u_1\} + A_2 \sin(\omega_2 t + \phi_2) \{u_2\}$$

From initial conditions

$$x_1(t) = \frac{1}{2} \sin\left(\sqrt{2}t + \frac{\pi}{2}\right) + \frac{1}{2} \sin\left(2t + \frac{\pi}{2}\right)$$

$$x_2(t) = \frac{3}{2} \sin\left(\sqrt{2}t + \frac{\pi}{2}\right) - \frac{3}{2} \sin\left(2t + \frac{\pi}{2}\right)$$

6. 연속계 (continuous system)

Discrete system	Continuous system
Finite DOF Ordinary differential equation ODE (t) Initial value problem Vector space (eigenvector)	

◆ Example : String

- Governing equation

$$\frac{\partial}{\partial x} \left[T(x) \frac{\partial y(x,t)}{\partial x} \right] = \rho(x) \frac{\partial^2 y(x,t)}{\partial t^2} \quad 0 < x < L \quad (10)$$

- boundary conditions (fixed-fixed conditions)

$$y(0,t) = y(L,t) = 0$$

Sol)

By separation of variables

$$y(x,t) = Y(x) F(t) \quad (11)$$

(11) \rightarrow (10), $\rho(x), T(x) = \text{constant}$

$$\frac{1}{\rho Y(x)} \frac{d}{dx} \left[T \frac{dY(x)}{dx} \right] = \frac{1}{F(t)} \frac{d^2 F(t)}{dt^2} \quad (12)$$

$$\left\{ \begin{array}{l} \frac{d^2 F(t)}{dt^2} + \omega^2 F(t) = 0 \\ -\frac{d}{dx} \left[T \frac{dY(x)}{dx} \right] = \omega^2 \rho Y(x) \\ Y(0) = Y(L) = 0 \end{array} \right. \quad \begin{array}{l} (13) \\ 0 < x < L \\ (14) \end{array}$$

From eq (14)

$$\begin{aligned} Y(x) &= A \sin \beta x + B \cos \beta x & \beta &= \omega \sqrt{\frac{\rho}{T}} \\ Y(0) &= B = 0 \\ Y(L) &= A \sin \beta L = 0 \end{aligned}$$

For non-trivial solution $\sin \beta L = 0$

$$\beta_r L = r \pi \quad r = 1, 2, 3, \dots$$

Natural frequency

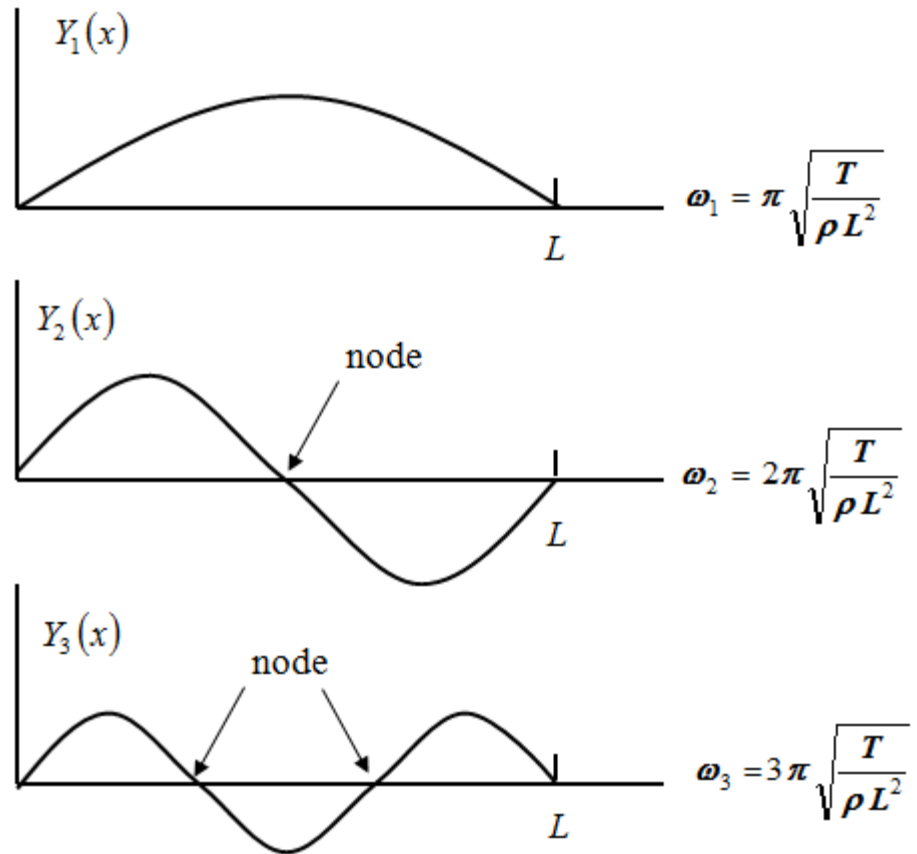
$$\omega_r = r \pi \sqrt{\frac{T}{\rho L^2}}$$

$$r = 1, 2, 3, \dots$$

Eigenfunction

$$Y_r = A_r \sin r \pi \frac{x}{L}$$

$$r = 1, 2, 3, \dots$$

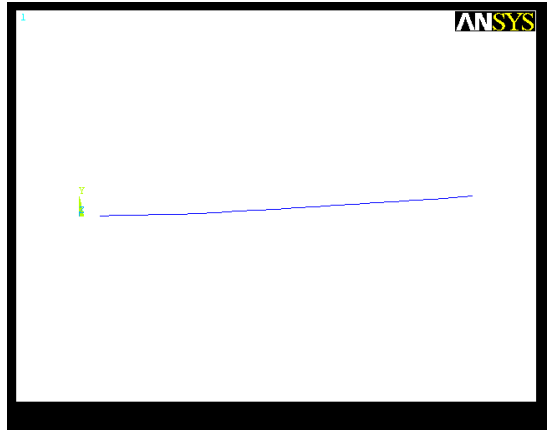


- Eigenfunctions of string -

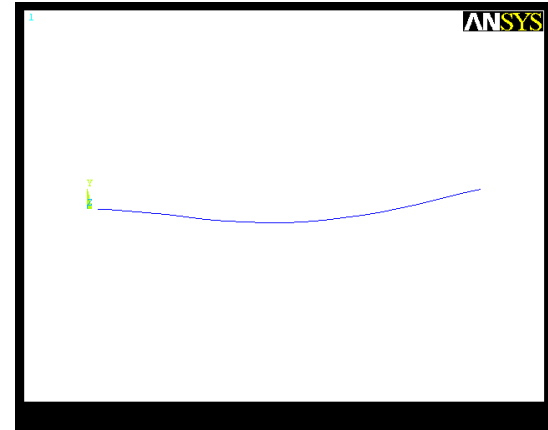
※ 유한요소 해석

◆ Example : Beam

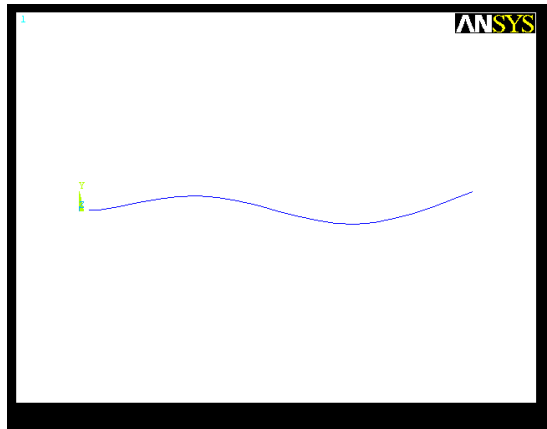
- First mode



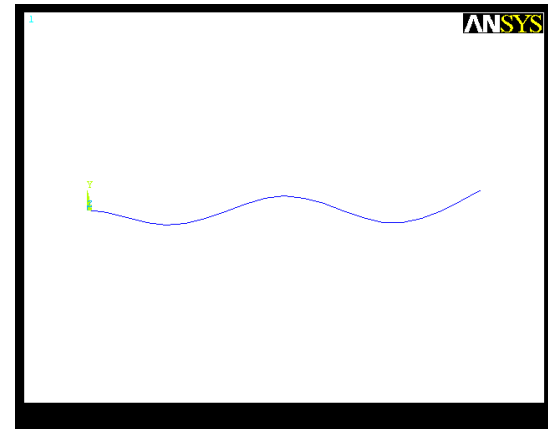
- Second mode



- Third mode

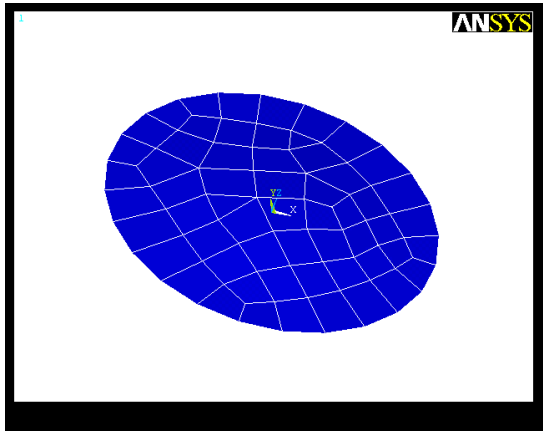


- Forth mode

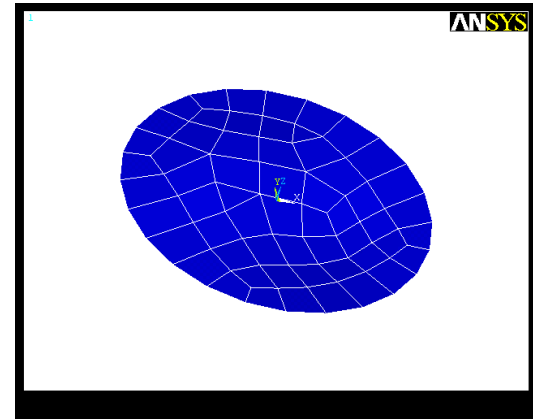


◆ Example : Disk

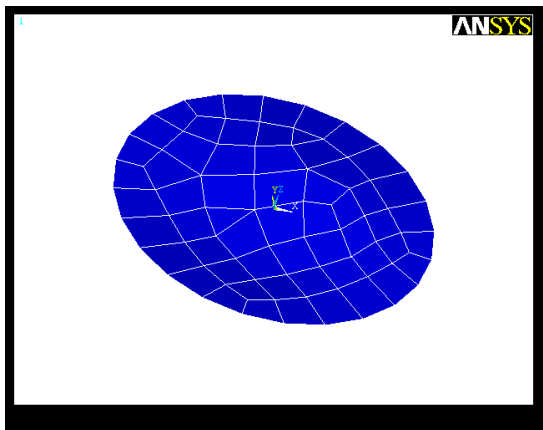
- First mode



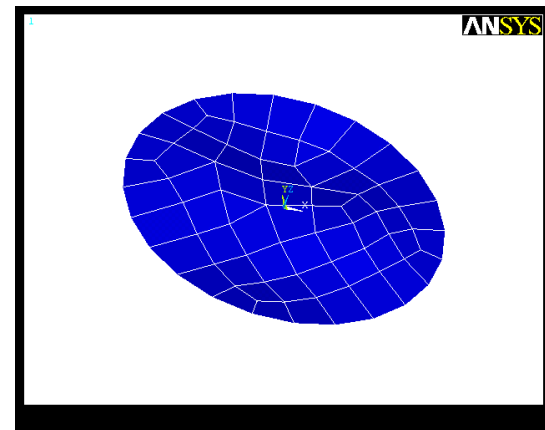
- Second mode



- Third mode

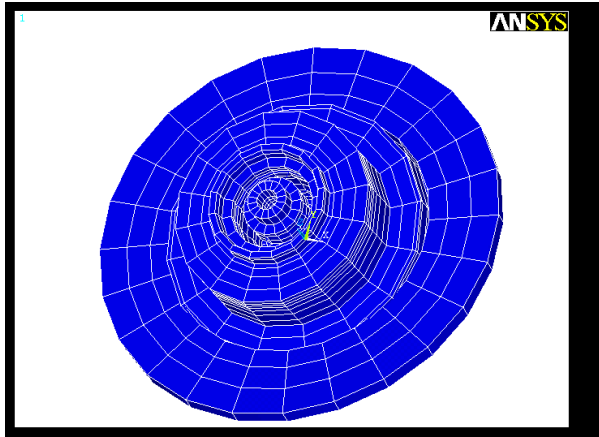


- Forth mode

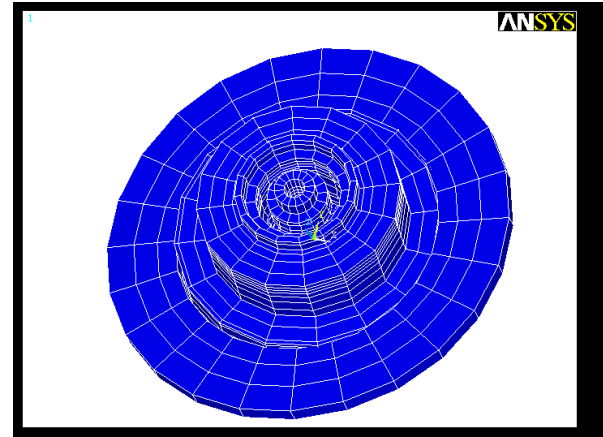


◆ Example : HDD

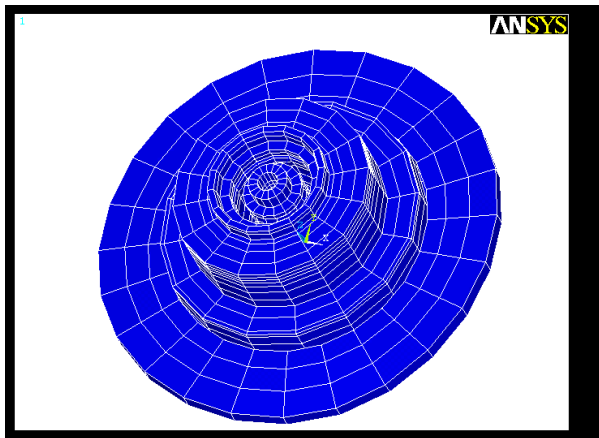
- First mode



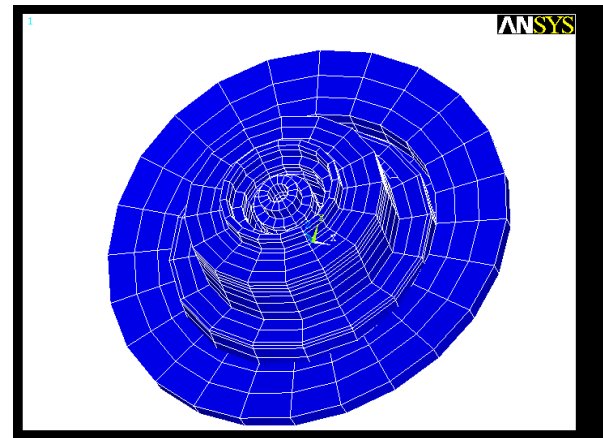
- Second mode



- Third mode

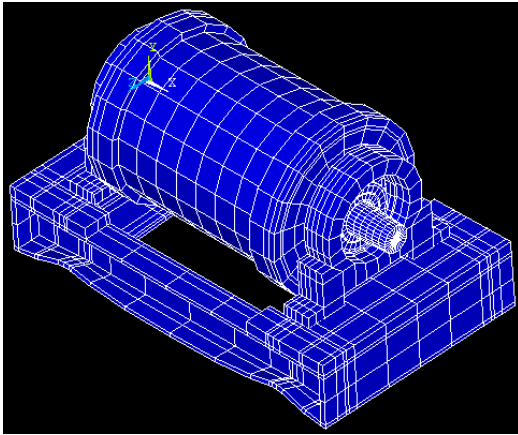


- Forth mode

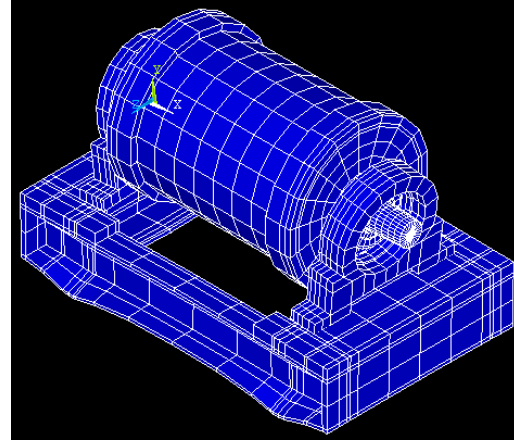


◆ Example : Dynamometer

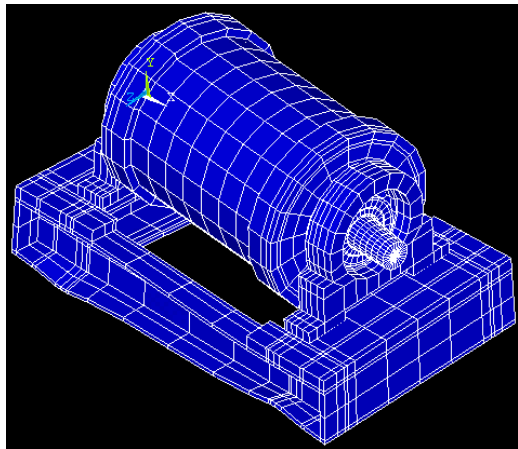
- First mode



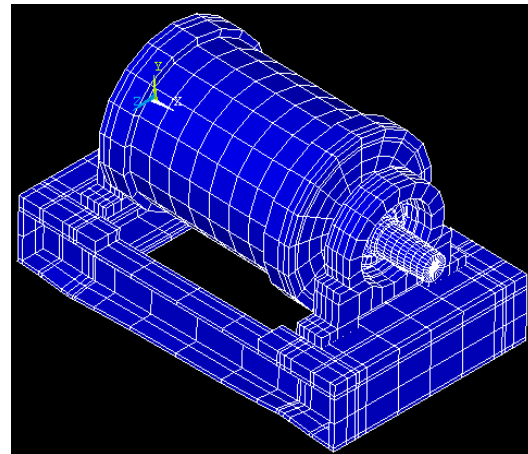
- Second mode



- Third mode

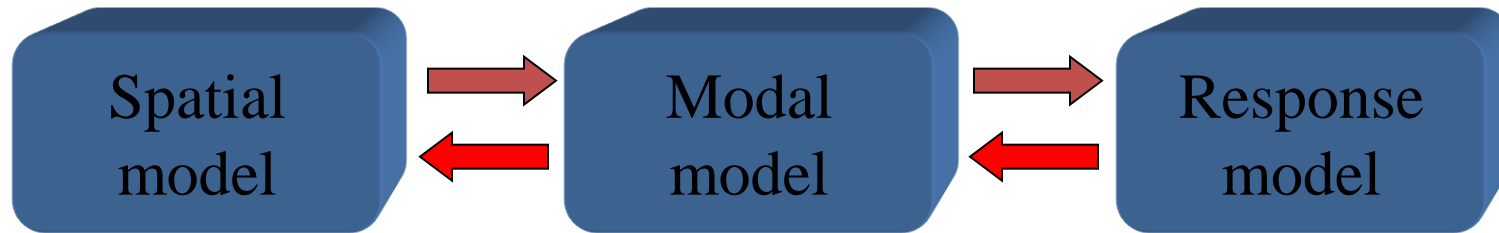


- Forth mode



7. 모달테스팅 (modal testing)

: processes involved in testing components or structures with the objective of obtaining a mathematical description of their dynamic or vibration behavior



Description of structure
- mass, spring, damper

Vibration mode
- natural frequencies
- mode shapes
- modal damping

Response level
- Frequency response function

(1) Basic measurement system

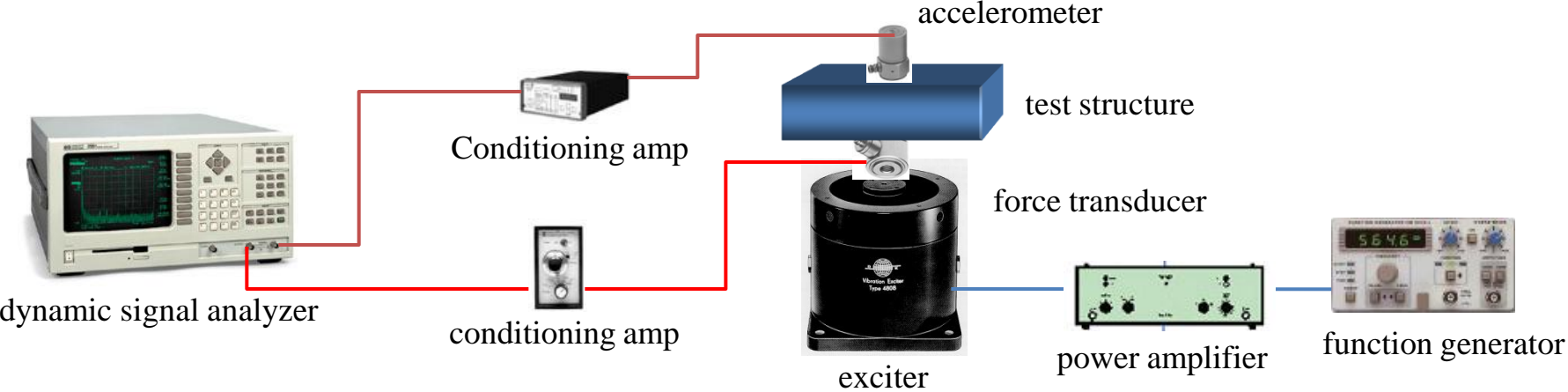
(1) Excitation system

(3) Amplifier

(2) Transduction system

(4) Analyzer(Dynamic signal analyzer)

(A) Shaker test



(B) Impact test

